

Amplitude-Phase Conversion Signal and Feature of its use in Practical Application

By

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Objective

Search methods for creating Two-frequency optical generator and development on the basis of their differential analysis techniques.

The main objective of the research:

1. Development and analysis of the properties of the amplitude-frequency conversion of coherent radiation.
2. Impact of two-frequency oscillations at the resonant system.
3. The implementation of the measuring system and the evaluation of its parameters.

Analysis of internal structure two-frequency oscillations

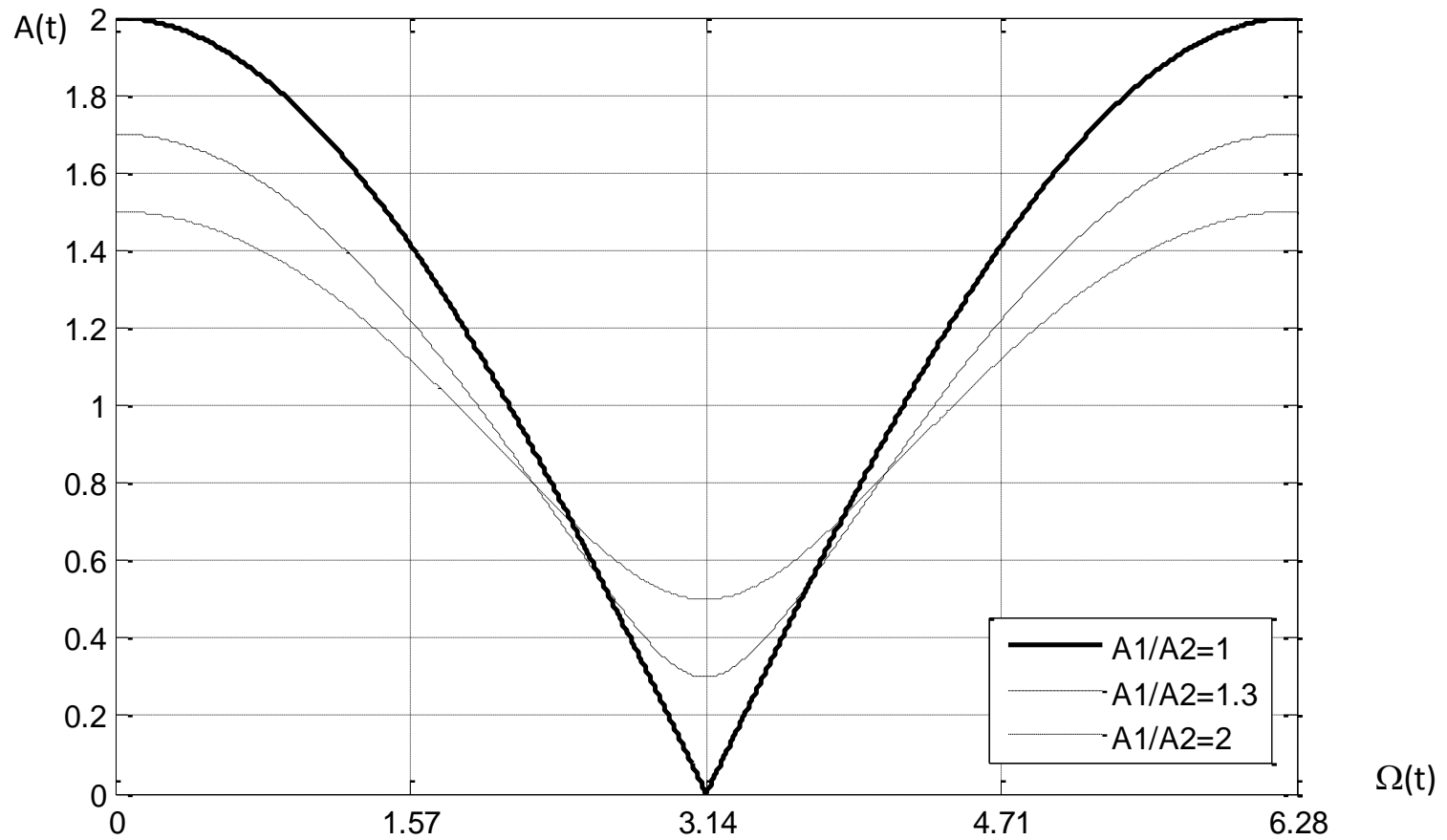
In general, the Two-frequency signal can be represented as:

$$U(t) = A_1 \cos(\omega_{01} t + \theta_1) + A_2 \cos(\omega_{02} t + \theta_2)$$

1- Investigation of the behavior of two-frequency signal instantaneous amplitude.

the value of the envelope of the two-frequency signal can be represented as:

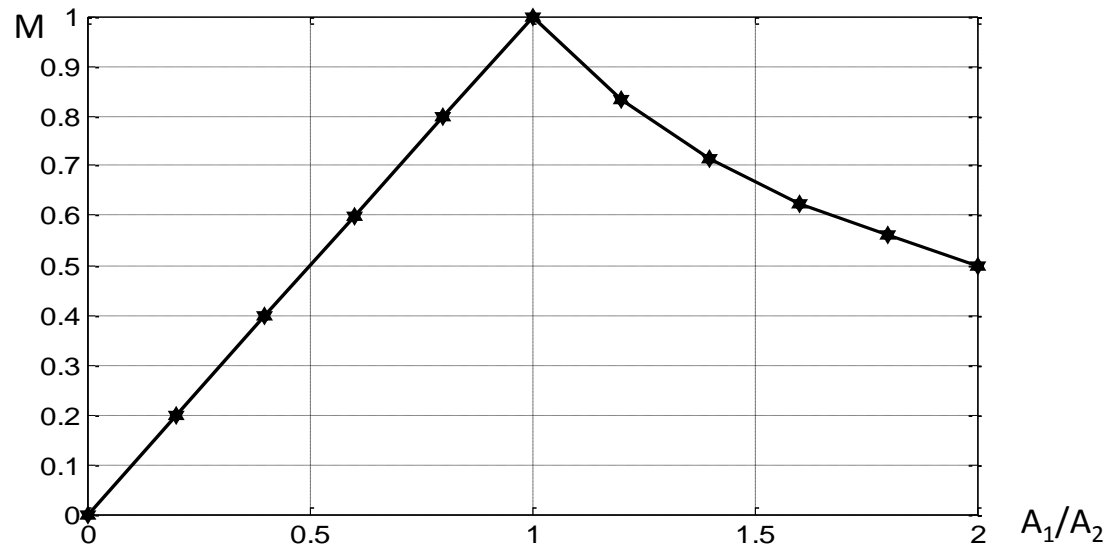
$$A(t) = \sqrt{A_1^2 + A_2^2 + 2A_1A_2 \cos(\Omega t)}$$



The $A(t)$ for different values of A_1 / A_2 .

$$M = 2(A_{\max} - A_{\min}) / 2(A_{\max} + A_{\min})$$

The results of calculations based on (A_1 / A_2) , we present in Fig.



Dependence of M (A₁ / A₂).

2-Investigation of the behavior of the instantaneous phase Two-frequency signals

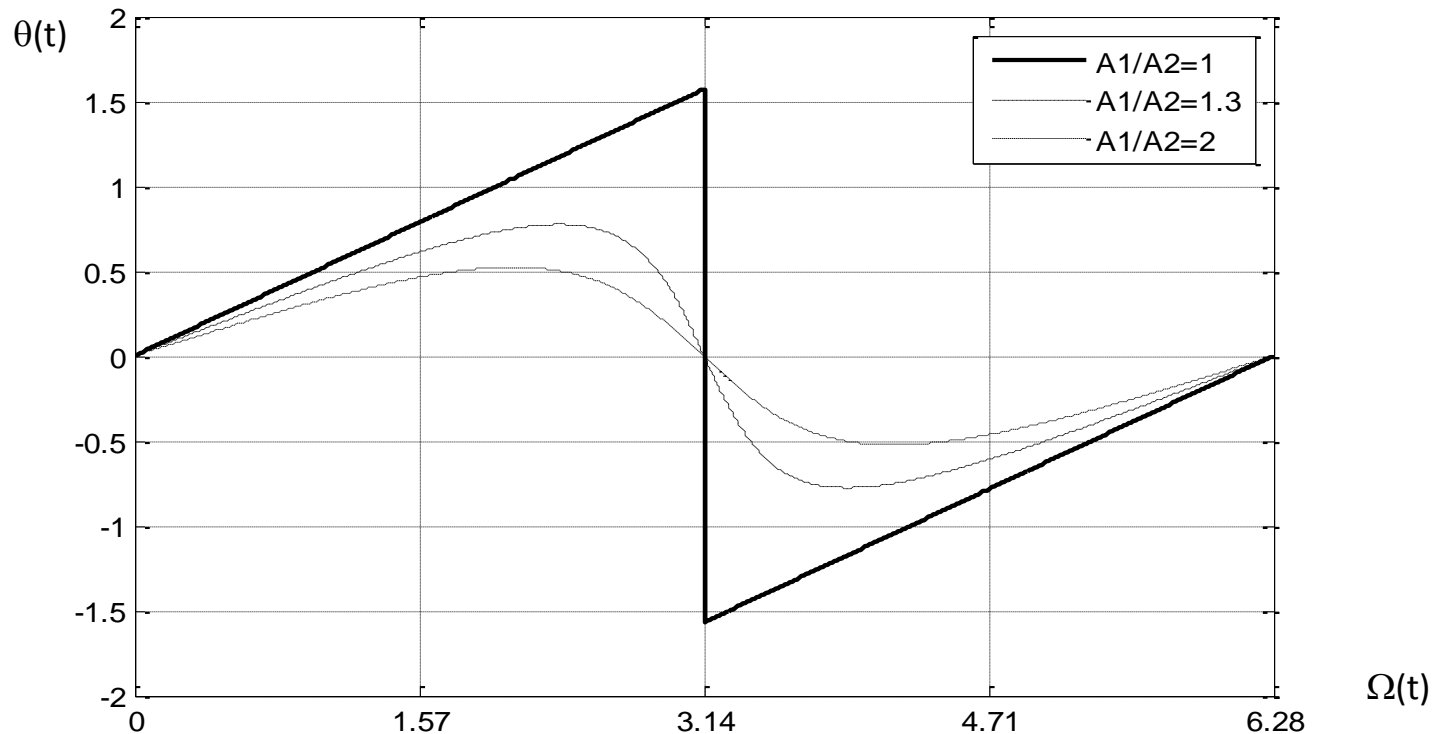
The instantaneous phase of the two-frequency signal when $\omega_{02} < \omega_{01}$, can be represented as:

$$\theta(t) = \text{arctg} \frac{\sin(\Omega t)}{A1 / A2 + \cos(\Omega t)}$$

The instantaneous phase of the two-frequency signal when $\omega_{02} > \omega_{01}$, can be represented as:

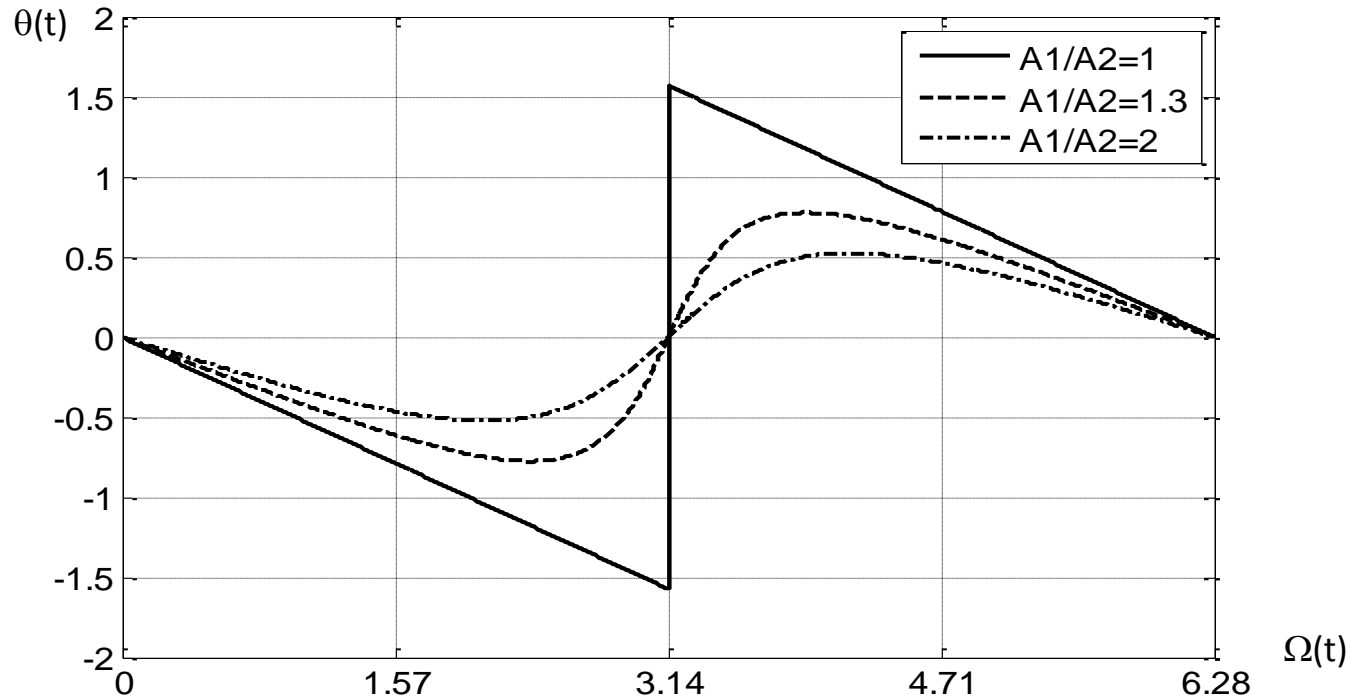
$$\theta(t) = -\text{arctg} \frac{\sin(\Omega t)}{A1 / A2 + \cos(\Omega t)}$$

The results of calculations based $\theta(t)$ for the case: $\omega_{01} > \omega_{02}$, shown in Fig.



Dependence $\theta(t)$ for the case $\omega_{01} > \omega_{02}$.

The results of calculations based $\theta(t)$ for the case: $\omega_{01} < \omega_{02}$, shown in Fig.



Dependence $\theta(t)$ for the case $\omega_{01} < \omega_{02}$.

3-Investigation of the behavior of the instantaneous frequency Two-frequency signal

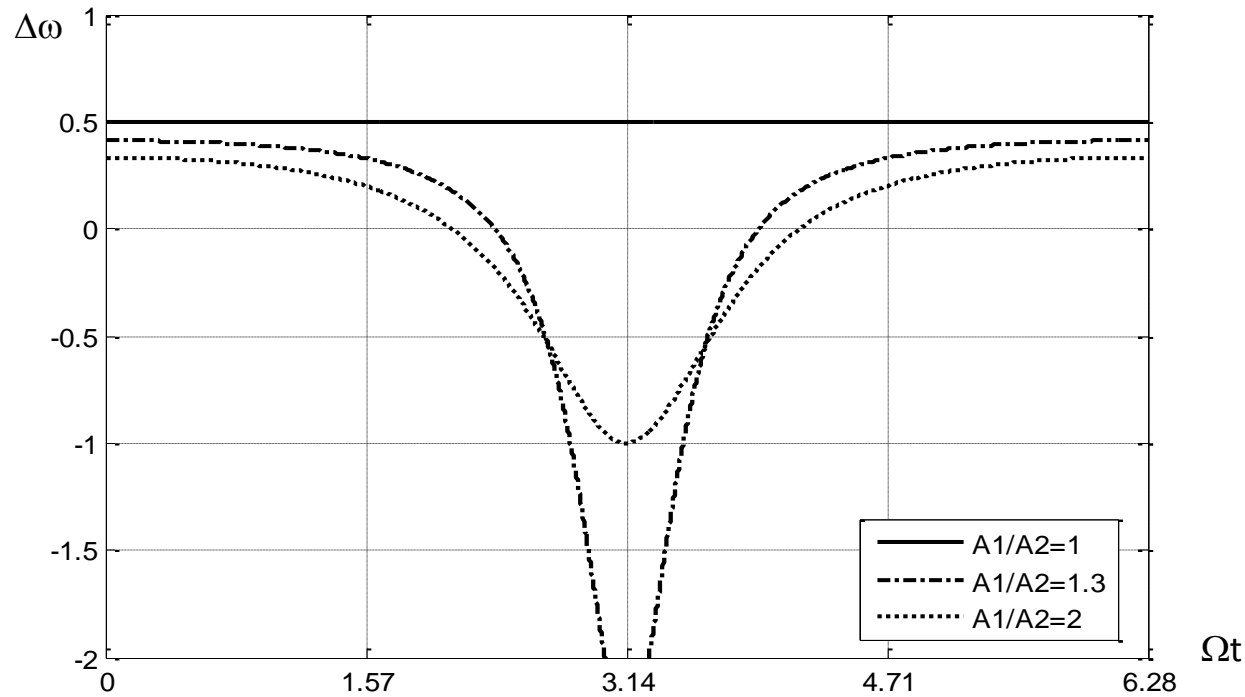
the expression for the instantaneous frequency of the two-frequency signal $\omega(t)$, when $\omega_{01} > \omega_{02}$

$$\omega_1(t) = \omega_{01}t - \left\{ \frac{\left[\frac{\cos(\Omega t)}{A1/A2 + \cos(\Omega t)} + \frac{\sin(\Omega t)^2}{(A1/A2 + \cos(\Omega t))^2} \right]}{\left[1 + \frac{\sin(\Omega t)^2}{(A1/A2 + \cos(\Omega t))^2} \right]} \right\}$$

the expression for the instantaneous frequency of the two-frequency signal $\omega(t)$, when $\omega_{01} < \omega_{02}$

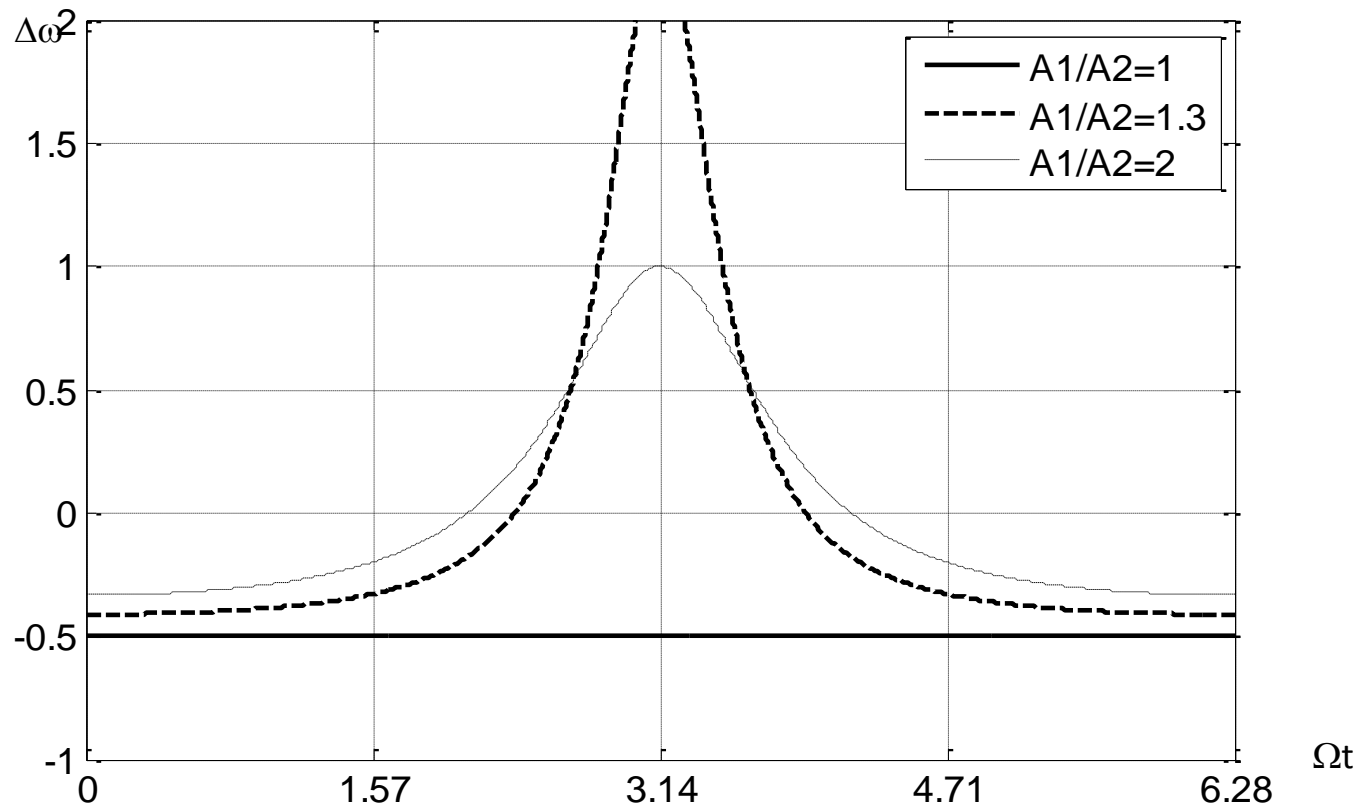
$$\omega_1(t) = \omega_{01}t + \left\{ \frac{\left[\frac{\cos(\Omega t)}{A1/A2 + \cos(\Omega t)} + \frac{\sin(\Omega t)^2}{(A1/A2 + \cos(\Omega t))^2} \right]}{\left[1 + \frac{\sin(\Omega t)^2}{(A1/A2 + \cos(\Omega t))^2} \right]} \right\}$$

The results of calculations based $\Delta\omega(t)$
at $\omega_{01} > \omega_{02}$, shown in Fig.



Dependence $\Delta\omega(t)$ at $\omega_{01} > \omega_{02}$.

The results of calculations based $\Delta\omega(t)$
at $\omega_{02} > \omega_{01}$, shown in Fig.



Dependence $\Delta\omega(t)$ at $\omega_{02} > \omega_{01}$.

The total expression for the two-frequency signal,
 When $(A_1 / A_2) \geq 1, \omega_{01} > \omega_{02}$

$$U(t) = \sqrt{A_1^2 + A_2^2 + 2A_1A_2\cos(\Omega t)}$$

$$\times \cos \left\{ \omega_{01} - \frac{\left[\frac{\cos(\Omega t)}{A_1 / A_2} + \frac{\sin(\Omega t)^2}{(A_1 / A_2 + \cos(\Omega t))^2} \right]}{\left[1 + \frac{\sin(\Omega t)^2}{(A_1 / A_2 + \cos(\Omega t))^2} \right]} + \operatorname{arctg} \frac{\sin(\Omega t)}{A_1 / A_2 + \cos(\Omega t)} \right\}$$

Impact two-frequency oscillations at the resonant system

Generalized amplitude-frequency characteristic of the oscillatory circuit whose input is fed a two-frequency signal can be determined from the following expression

$$Y_{(\varepsilon)} = \frac{1}{\sqrt{1 + \varepsilon^2_{0k}}}$$

where $\varepsilon_{0k} = Q(\omega/\omega_0 - \omega_0/\omega)$ - generalized detuning of the oscillating circuit

generalized detuning of the first component of the output signal

$$\varepsilon_{01} = \varepsilon_0 + \Delta\varepsilon/2$$

$$A_{1out}(\varepsilon_{01}) = \frac{1}{\sqrt{1 + (\varepsilon_0 + \Delta\varepsilon/2)^2}}$$

generalized detuning of the second component of the output signal

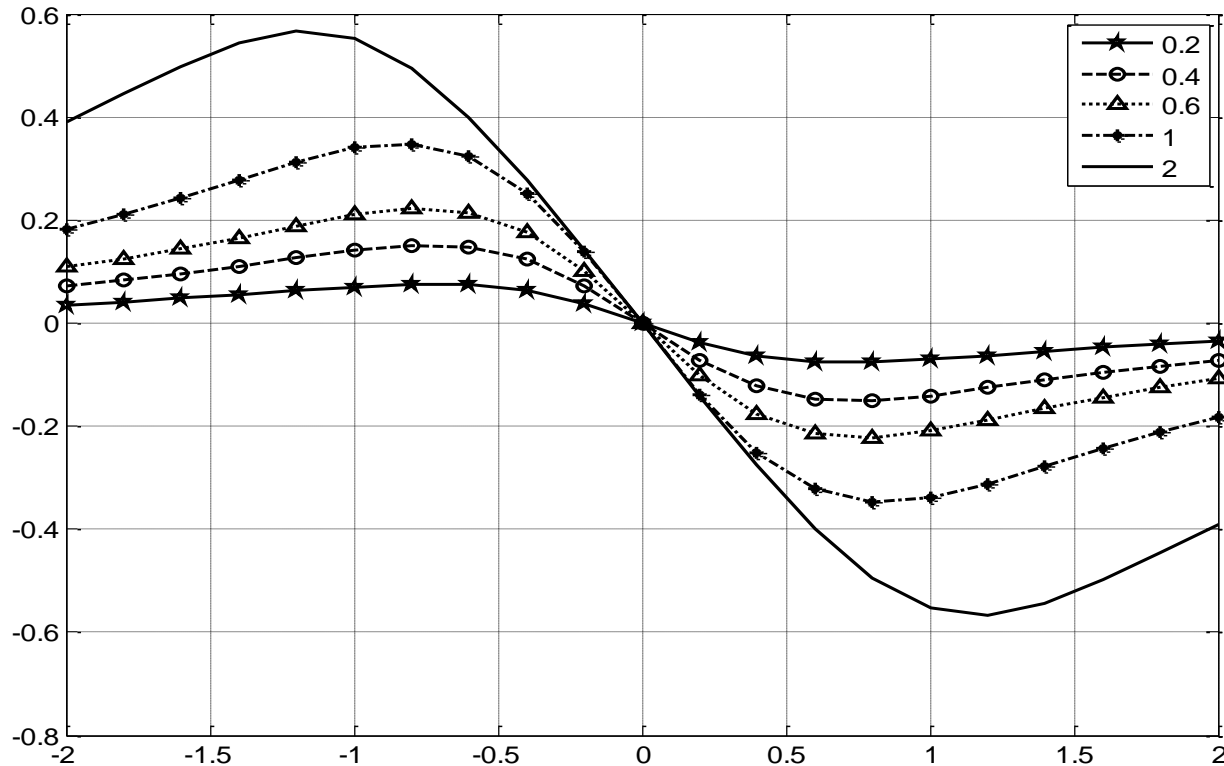
$$\varepsilon_{02} = \varepsilon_0 - \Delta\varepsilon/2$$

$$A_{2out}(\varepsilon_{02}) = \frac{1}{\sqrt{1 + (\varepsilon_0 - \Delta\varepsilon/2)^2}}$$

the difference between the amplitudes of the first and second components of the two-frequency output signal ΔA_{out} is given by type

$$\Delta A_{out} = \frac{1}{\sqrt{1 + (\varepsilon_0 + \Delta\varepsilon/2)^2}} - \frac{1}{\sqrt{1 + (\varepsilon_0 - \Delta\varepsilon/2)^2}}$$

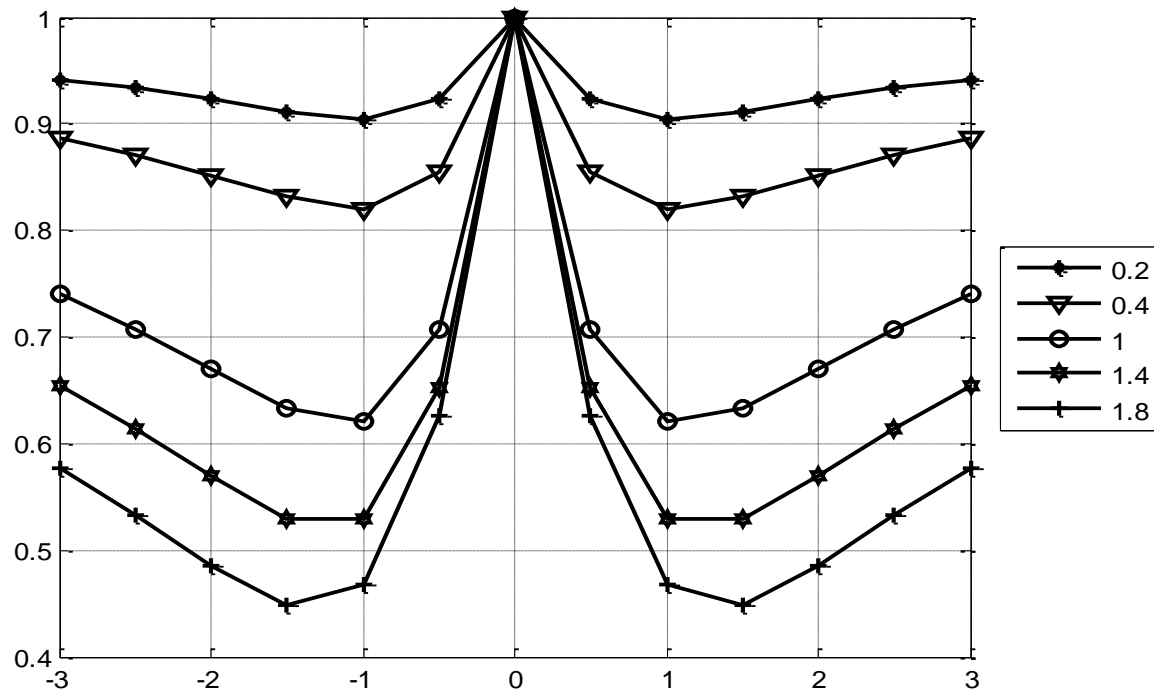
The results of calculations based $\Delta A_{\text{out}}(\varepsilon_0)$ for different values $\Delta\varepsilon$ [0.1; 0.2; 0.4; 1; 2]



Dependence $\Delta A_{\text{out}}(\varepsilon_0)$ for different values $\Delta\varepsilon$.

modulation index envelope of the two-frequency output signal is the ratio of the amplitudes of its components

$$M = \frac{\sqrt{1 + (\varepsilon_0 + \Delta\varepsilon/2)^2}}{\sqrt{1 + (\varepsilon_0 - \Delta\varepsilon/2)^2}}$$

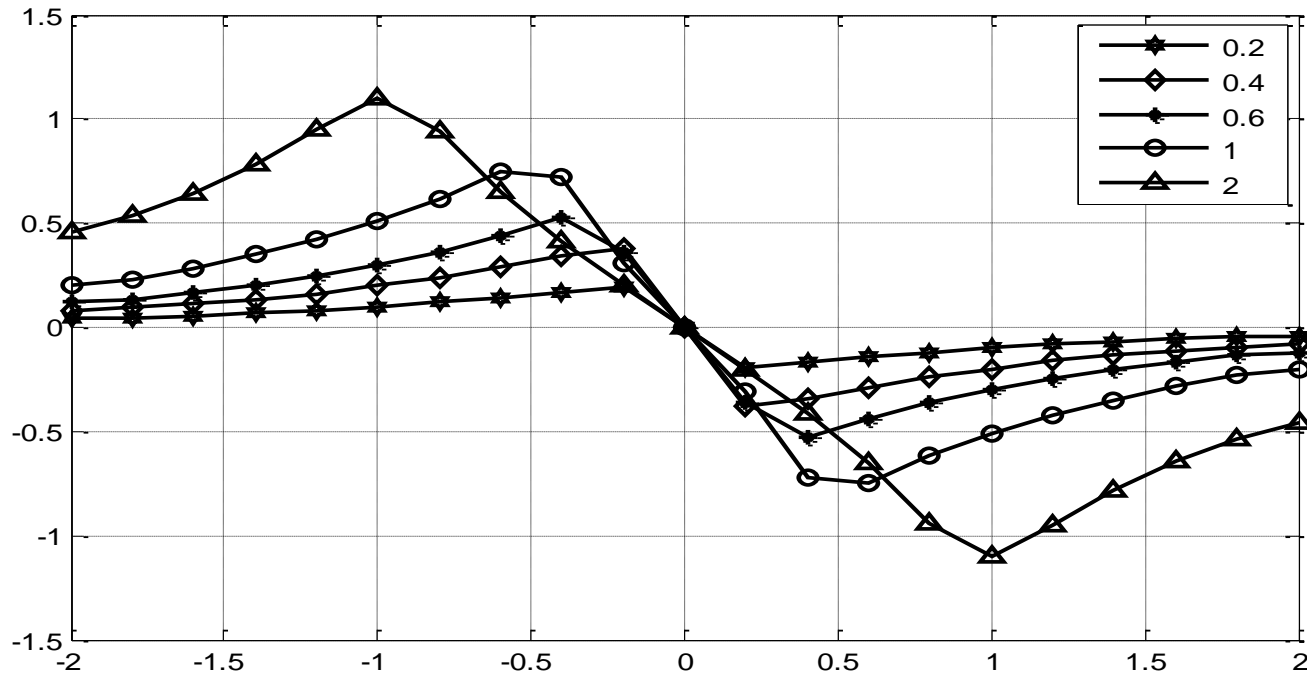


The dependence of $m(\varepsilon_0)$ at different values $\Delta\varepsilon$

Result to the phase difference components

$(\varphi_{2\text{out}} - \varphi_{1\text{out}})$, phase shift occurs envelope

$$\Delta\varphi(\varepsilon_0) = [-\text{arctg}(\varepsilon_0 - \Delta\varepsilon/2)] - [-\text{arctg}(\varepsilon_0 + \Delta\varepsilon/2)]$$



Dependence $\Delta\varphi(\varepsilon_0)$ for different values $\Delta\varepsilon$.

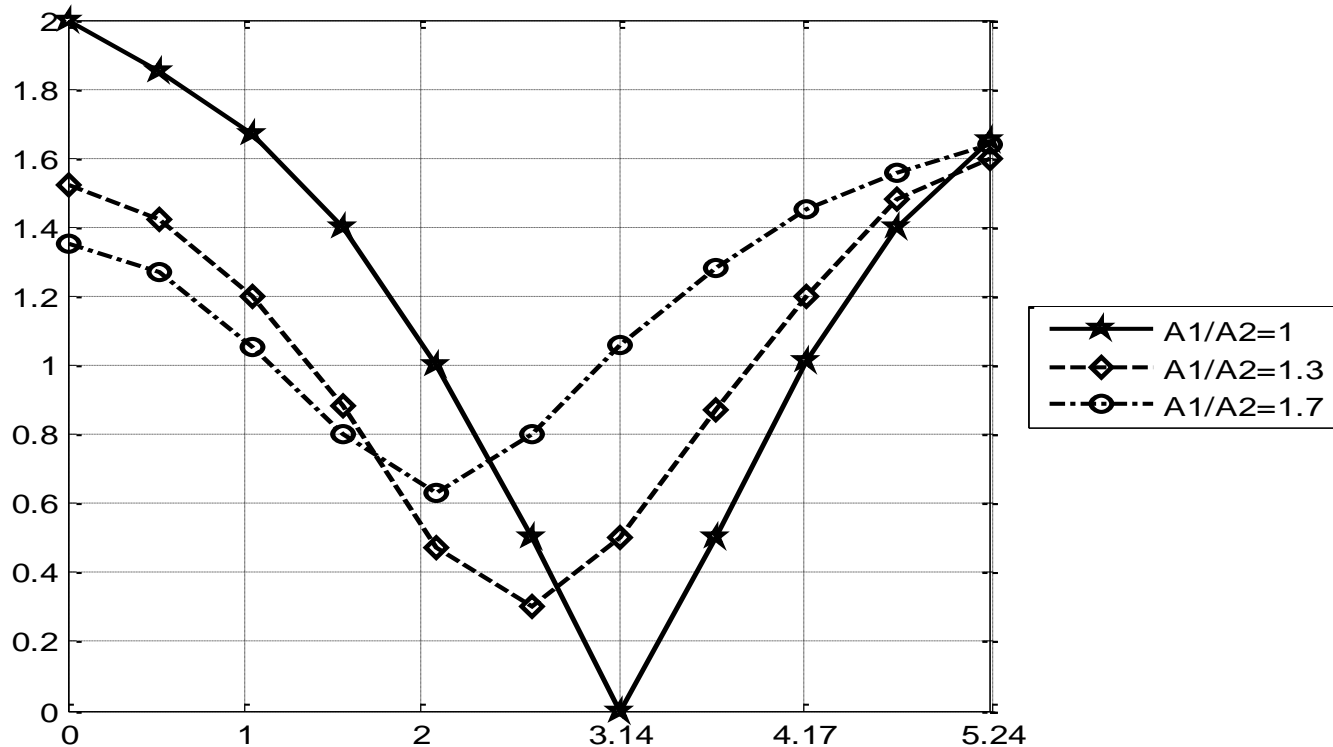
The total expression for the two-frequency output signal with the series resonant circuit

$$-\infty < \varepsilon_0 < -\varepsilon_0/2: \varepsilon_{01} > \varepsilon_{02}, \quad A_1/A_2 > 1$$

$$U_{\text{свix}}(t) = \sqrt{A_1^2_{\text{свix}} + A_2^2_{\text{свix}} + 2A_1A_2_{\text{свix}} \cos [(\varphi_{2\text{свix}} - \varphi_{1\text{свix}}) + \Omega(t)]} \times$$

$$\times \cos (\omega_M(t) + \left\{ \varphi_1 + \operatorname{arctg} \left[\frac{\operatorname{Sin} [(\varphi_{2\text{свix}} - \varphi_{1\text{свix}}) + \Omega(t)]}{A_1A_2_{\text{свix}} / A_2A_2_{\text{свix}} + \cos [(\varphi_{2\text{свix}} - \varphi_{1\text{свix}}) + \Omega(t)]} \right] \right\})$$

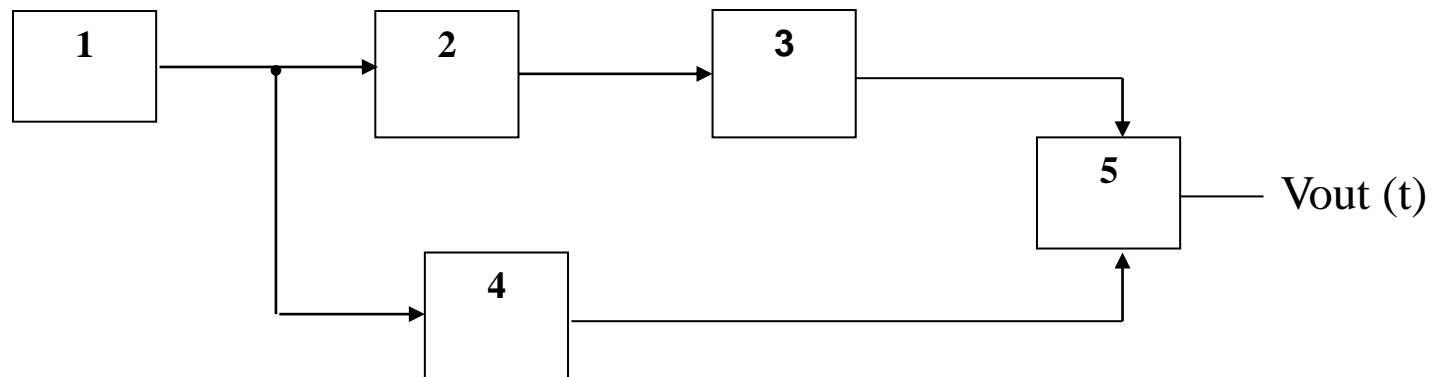
The results of calculations of the envelope of the output signal show



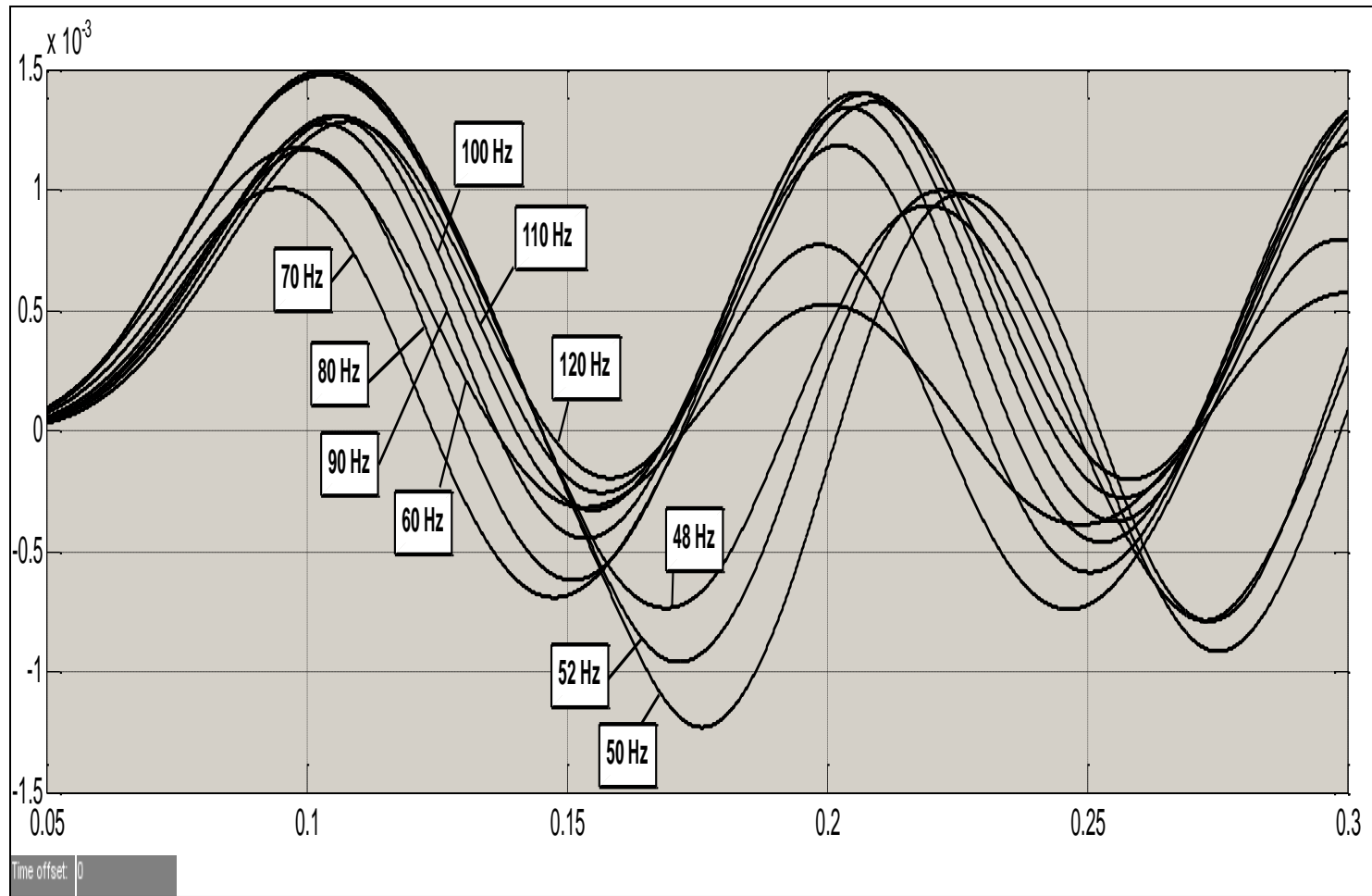
The envelope of the two-frequency output signal $V_{out}(t)$ in the series resonant circuit **when** $-\infty < \varepsilon_0 < -\varepsilon_0/2$: $\varepsilon_{01} > \varepsilon_{02}$, $A_1/A_2 > 1$.

Technical measuring systems on resonant two-frequency signals

Two-frequency tuning method of resonant systems in the one-sided approach to the resonance



1- Two-frequency signal generator , 2 - resonance system , 3&4 - amplitude detector 5 - phase detector



The result of the scheme for the simulation of different signals after the phase detector

Thank you